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54 Integrated amplifier with an accurately defined gain factor.

57 The invention provides an integrated amplifier whose gain factor (A_s) is adjusted by means of an auxiliary amplifier (2). The gain factor (A_s) is determined by the ratio of two on-chip resistors (R_1 , R_2) and by the ratio of the dimensions of transistors in long-tailed pair circuits (6-2 ... 6-N) in the signal amplifier (3) to those of the transistors in the long-tailed pair circuit (6-1) in the auxiliary amplifier (2). Both resistance ratios and ratios between complete circuits can be realised highly accurately in inte-

grated circuits. As a result, the accuracy of the gain factor (A_s) is great. In an embodiment of the invention the dimensions of the long-tailed pair circuits (6-1 ... 6-N) in the auxiliary amplifier (2) and in the signal amplifier (3) are the same. This achieves that if the adjusting voltages and adjusting currents of corresponding transistors in the long-tailed pair circuits (6-1 ... 6-N) are the same, the gain factor (A_s) is over a large range independent of supply voltage and temperature.

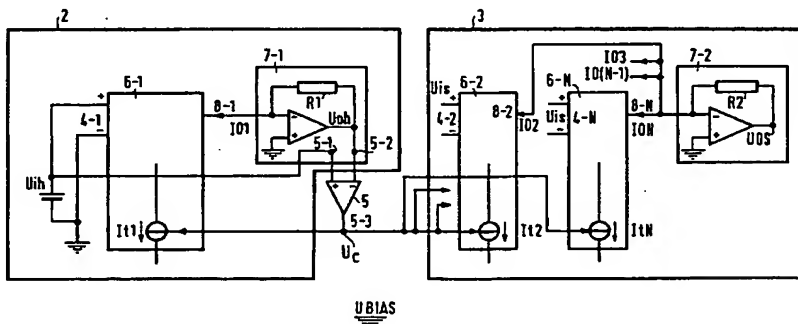


FIG.1

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The invention relates to an integrated amplifier comprising an auxiliary amplifier which includes a first long-tailed pair circuit having an input for receiving an auxiliary voltage, a signal amplifier which includes at least a second long-tailed pair circuit having an input for receiving a signal voltage to be amplified, and adjusting means for adjusting, via a tail current from at least the second long-tailed pair circuit, a gain factor of the signal amplifier in response to the value of an output current of the first long-tailed pair circuit.

An integrated amplifier of this type may be used, for example, as a microphone preamplifier in a transmission IC for wire telephony. In that field there is an important requirement that the gain factor be accurately defined.

An integrated amplifier as described in the opening paragraph is known from US 4,489,282. In the amplifier described in that document the output current of the first long-tailed pair circuit is compared with an external reference current. The tail current of one or more long-tailed pair circuits in the signal amplifier is adjusted on the basis of the difference between these currents. The external reference current is dependent on an off-chip resistor. External resistors can be obtained with any desired accuracy. This provides great accuracy of the gain factor to be adjusted. A drawback of the amplifier described in that document is that it is not fully integrable and, therefore, relatively expensive due to the presence of the off-chip resistor.

It is an object of the invention to provide an integrated amplifier of the type defined in the opening paragraph in which said drawback is obviated and which can be realised in a simple and cost-effective manner while an accurately defined gain factor is retained. An amplifier having an accurate gain factor can be realised, it is true, by adjusting the gain factor with two or four resistors in known manner. A drawback of this is that if a high input impedance is desired, which is the case for a microphone preamplifier, the noise of the resistors starts playing a role that cannot be discarded.

An integrated amplifier according to the invention is therefore characterized in that the adjusting means comprise a first current-voltage converter coupled to the first long-tailed pair circuit for converting, by means of a first resistor, the output current of the first long-tailed pair circuit to an output voltage of the auxiliary amplifier and comprise a comparator element for comparing a voltage proportional to the auxiliary amplifier output voltage with a voltage proportional to the auxiliary voltage, the output of the comparator element being coupled to control electrodes of tail current transistors of the long-tailed pair circuits in the auxiliary amplifier and the signal amplifier, and in that the at least second long-tailed pair circuit is

coupled to a second current-voltage converter for converting an output current of the at least second long-tailed pair circuit to an output voltage of the signal amplifier by means of a second resistor.

The accuracy of the gain factor of the amplifier is determined by the ratio between the second and the first resistance and by the ratio of the dimensions of the transistors in the long-tailed pair circuits in the signal amplifier to those of the transistors in the long-tailed pair circuit in the auxiliary amplifier. This gain factor is accurately defined because resistance ratios or ratios of complete on-chip circuits can be realised with great accuracy. Since all the elements of the amplifier are manufactured in a fully integrated manner, the amplifier is relatively low priced.

An embodiment of the integrated amplifier is therefore characterized in that the signal amplifier comprises a plurality of parallel-arranged long-tailed pair circuits whose transistors have the same dimensions as the transistors in the long-tailed pair circuit in the auxiliary amplifier and whose outputs are coupled to the second current-voltage converter.

This integrated amplifier can be easily manufactured because all long-tailed pair circuits are the same. Since corresponding transistors in the auxiliary amplifier and signal amplifier have the same dimensions, adjusting voltages and adjusting currents, the gain factor will over a large range be independent of the supply voltage.

The invention will be further explained with reference to a drawing in which:

Fig. 1 shows an integrated amplifier according to the invention,

Fig. 2 shows a general diagram of a long-tailed pair circuit in detail, and

Fig. 3 shows how the input and output variables of a long-tailed pair circuit are mutually related.

Fig. 1 shows an integrated amplifier according to the invention, which comprises both an auxiliary amplifier 2 and a signal amplifier 3. The auxiliary amplifier 2 includes a first long-tailed pair circuit 6-1 having an input 4-1 for receiving an auxiliary voltage U_{ih} and an output 8-1 on which an output current I_{01} is present. Fig. 2 shows a general diagram of a long-tailed pair circuit 6 in detail. There should be observed that this is only one of the possibilities of arranging such a circuit. The transistors T1 and T2 have the same dimensions as transistors T3 and T4. They are connected in such a way that current I1 is equally large as I2. By applying an input voltage U_i between the control electrodes E4 and E3 of the transistors T4 and T3, a current I3 will start flowing through transistor T4 which is larger than the current I1 flowing through transistor T3. The difference between the two currents I3 and I2 is output current I0. The transcon-

ductance g_m of the long-tailed pair circuit 6 is equal to dl/dU_i by definition. The tail current I_t determines how large the currents flowing through the long-tailed pair circuit 6 are. The magnitude of this tail current I_t may be affected by adjusting a tail current transistor T_t by a control electrode E_c . As a result, the magnitude of the transconductance g_m is affected. Fig. 3 shows how the input and output parameters of the long-tailed pair circuit 6 are mutually related. When the circuit is adjusted between the input voltages U_{i1} and U_{i2} , the output current I_O linearly depends on the input voltage U_i . In this range, called the linear range, the transconductance g_m is thus equal to I_O/U_i . Since the curve runs through origin, the transconductance g_m in the linear range is constant. The magnitude of this transconductance g_m depends on the quantity of the tail current I_t and, in the case where MOS transistors are used, the width-to-length ratio of the transistors in the long-tailed pair circuit 6.

As shown in Fig. 1, the output 8-1 of the first long-tailed pair circuit 6-1 (the second digit in the reference number designating which long-tailed pair circuit shown in Fig. 1 is discussed) is coupled to a first current-voltage converter 7-1 for converting an output current I_{O1} of the first long-tailed pair circuit 6-1 to an output voltage U_{oh} of the auxiliary amplifier 2 by means of a first resistor R_1 . A comparator element 5 compares this output voltage U_{oh} or a voltage related thereto and obtained, for example, by means of a voltage divider, with the auxiliary voltage U_{ih} applied to the first long-tailed pair circuit 6-1, or with a voltage related thereto and likewise obtained, for example, by means of a voltage divider (not shown). In response to an output voltage U_c of the comparator element 5 a tail current I_{t1} of the first long-tailed pair circuit 6-1 is controlled, so that the transconductance g_{m1} of the first long-tailed pair circuit 6-1 is affected. As long as the auxiliary voltage U_{ih} or the voltage related thereto exceeds the output voltage U_{oh} of the auxiliary amplifier 2 or the voltage related thereto, the tail current I_{t1} and hence also the transconductance g_{m1} and the output current I_{O1} of the first long-tailed pair circuit 6-1 increase. As a result, also the output voltage U_{oh} of the auxiliary amplifier 2 or the voltage related thereto increases. This process is continued until the voltages on the inputs 5-1 and 5-2 of the comparator element 5 have equal values. If the output voltage U_{oh} of the auxiliary amplifier 2 or the voltage related thereto exceeds the auxiliary voltage U_{ih} or the voltage related thereto, the tail current I_{t1} is reduced, so that the transconductance g_{m1} and the output current I_{O1} of the first long-tailed pair circuit 6-1 and hence also the output voltage U_{oh} of the auxiliary amplifier 2 decrease. This process too is continued until the voltages on the inputs 5-1 and 5-2 of the

comparator element 5 are equal. In this state of balance the gain factor A_h of the auxiliary amplifier 2 assumes a specific value. If the output voltage U_{oh} of the auxiliary voltage U_{ih} as shown in the drawing Figure are directly applied to the comparator element 5, this gain factor $A_h = 1$. This means that in this case $g_{m1} = 1/R_1$ holds for the transconductance g_{m1} of the first long-tailed pair circuit 6-1, which is equal to I_{O1}/U_{ih} in the linear range. with respect to Fig. 2 there can be observed that the auxiliary voltage U_{ih} need not be accurate. The auxiliary voltage U_{ij} to be supplied should not be selected too large, because otherwise the transconductance g_{m1} ends up outside the linear range. Too small a value of the auxiliary voltage U_{ij} is not desired either, because in that case undesired effects such as the input offset voltage may start playing too large a role. This effect may be eliminated by reversing the polarity of the input voltage U_i and changing the switching mode of the transistors T_1 and T_2 with a certain frequency as described in the publication "Dual Tone and Modem Frequency Generator with On-Chip Filters and Voltage Reference" by Walter Oswald and Jaap Mulder in "IEEE Journal of Solid State Circuits, Vol. SC-19, No. 3" June 1984.

The operation of the signal amplifier 3 is similar to that of the auxiliary amplifier 2. The signal voltage U_{is} to be amplified is applied to the inputs 4-2 ... 4-N of the long-tailed pair circuits 6-2 ... 6-N in the signal amplifier 3. The outputs of these long-tailed pair circuits 6-2 ... 6-N are coupled to a second current-voltage converter 7-2 for converting output currents I_{O2} ... I_{ON} of the long-tailed pair circuits 6-2 ... 6-N to an output voltage U_{OS} of the signal amplifier 3 by means of a second resistor R_2 .

The output voltage U_c of the comparator element 5 is also used for controlling one or more tail currents I_{t2} ... I_{tN} of long-tailed pair circuits 6-2 ... 6-N in the signal amplifier 3. This is effected to adjust the transconductances g_{m1} ... g_{mN} of the long-tailed pair circuits 6-2 ... 6-N and hence the gain factor A_s of the signal amplifier 3. As for this structure the long-tailed pair circuits 6-2 ... 6-N in the signal amplifier 3 are identical with the long-tailed pair circuit 6-1 in the auxiliary amplifier 2. Only the dimensions of the transistors in the long-tailed pair circuits 6-2 ... 6-N may be different from the dimensions of the transistors in the first long-tailed pair circuit 6-1. The ratio of input to output values of each long-tailed pair circuit 6-2 ... 6-N in the signal amplifier 3 shows the same variation as the ratio of the input to output values of the first long-tailed pair circuit 6-1 as shown in Fig. 2, because these circuits are all of identical structure. Only the slopes of the curves may differ as a result of differences in dimensions of the transistors in

the various circuits.

Since the long-tailed pair circuits 6-1 ... 6-N are all deposited on the same chip, their properties are mutually equal to within narrow limits. Since the structure of all the long-tailed pair circuits 6-1 ... 6-N is the same, an adjustment of the transconductance g_{m1} of the first long-tailed pair circuit 6-1 of the auxiliary amplifier 2 results in the transconductances $g_{m2} \dots g_{mN}$ of the long-tailed pair circuits 6-2 ... 6-N of the signal amplifier 3 being adjusted to within the same range. The transconductances $g_{m2} \dots g_{mN}$ *per se* cannot be made accurate, because they depend on the on-chip resistor R1, but by supplying the output currents I02 ... I0N of the long-tailed pair circuits 6-2 ... 6-N from the signal amplifier 3 to a second current-voltage converter 7-2 for conversion to an output voltage U0S of the signal amplifier 3 by means of a second on-chip resistor R2, the gain factor A_s of this signal amplifier 3 is solely made dependent on the resistance ratio $R2/R1$ and on the ratio of the dimensions of the transistors in the long-tailed pair circuits 6-2 ... 6-N in the signal amplifier 3 to those of the transistors in the long-tailed pair circuit 6-1 in the auxiliary amplifier 2. Since the resistors R1 and R2 are manufactured in a same process, their ratio is accurately reproducible. Ratios of complete circuits are likewise accurately reproducible on-chip, so that the invention provides an integrated amplifier whose gain factor A_s is accurately defined. The noise, if any, generated in the auxiliary amplifier 2 is applied to the signal amplifier 3 in common mode and thus strongly suppressed.

Highly advantageous is the embodiment in which all long-tailed pair circuits 6-2 ... 6-N in the signal amplifier 3 are exactly the same as the first long-tailed pair circuit 6-1 in the auxiliary amplifier 2. In that case there are no differences in transistor dimensions in the long-tailed pair circuits 6-1 ... 6-N, which provides that the integrated amplifier can easily be made accurate. In this embodiment the gain factor A_s of the signal amplifier 3 is over a large range independent of the supply voltage and temperature.

Claims

1. Integrated amplifier comprising an auxiliary amplifier (2) which includes a first long-tailed pair circuit (6-1) having an input (4-1) for receiving an auxiliary voltage (U_{ih}), a signal amplifier (3) which includes at least a second long-tailed pair circuit (6-2) having an input (4-2) for receiving a signal voltage (U_{is}) to be amplified, and adjusting means for adjusting, via a tail current (I02) from at least the second long-tailed pair circuit (6-2), a gain factor (A_s) of the signal amplifier (3) in response to the

value of an output current (I01) of the first long-tailed pair circuit (6-1), characterized in that the adjusting means comprise a first current-voltage converter (7-1) coupled to the first long-tailed pair circuit (6-1) for converting, by means of a first resistor (R1), the output current (I01) of the first long-tailed pair circuit (6-1) to an output voltage (U_{0h}) of the auxiliary amplifier (2) and comprise a comparator element (5) for comparing a voltage proportional to the output voltage (U_{0h}) of the auxiliary amplifier (2) with a voltage proportional to the auxiliary voltage (U_{ih}), the output (5-3) of the comparator element (5) being coupled to control electrodes ($E_{c1} \dots E_{cN}$) of tail current transistors ($T_{t1} \dots T_{tN}$) of the long-tailed pair circuits (6-1 ... 6-N) in the auxiliary amplifier (2) and the signal amplifier (3), and in that the at least second long-tailed pair circuit (6-2) is coupled to a second current-voltage converter (7-2) for converting an output current (I02) of the at least second long-tailed pair circuit (6-2) to an output voltage (U_{0s}) of the signal amplifier (3) by means of a second resistor (R2).

2. Integrated amplifier as claimed in Claim 1, characterized in that the signal amplifier (3) comprises a plurality of parallel-arranged long-tailed pair circuits (6-2 ... 6-N) whose transistors have the same dimensions as the transistors in the long-tailed pair circuit (6-1) in the auxiliary amplifier (2) and whose outputs (8-2 ... 8-N) are coupled to the second current-voltage converter (7-2).

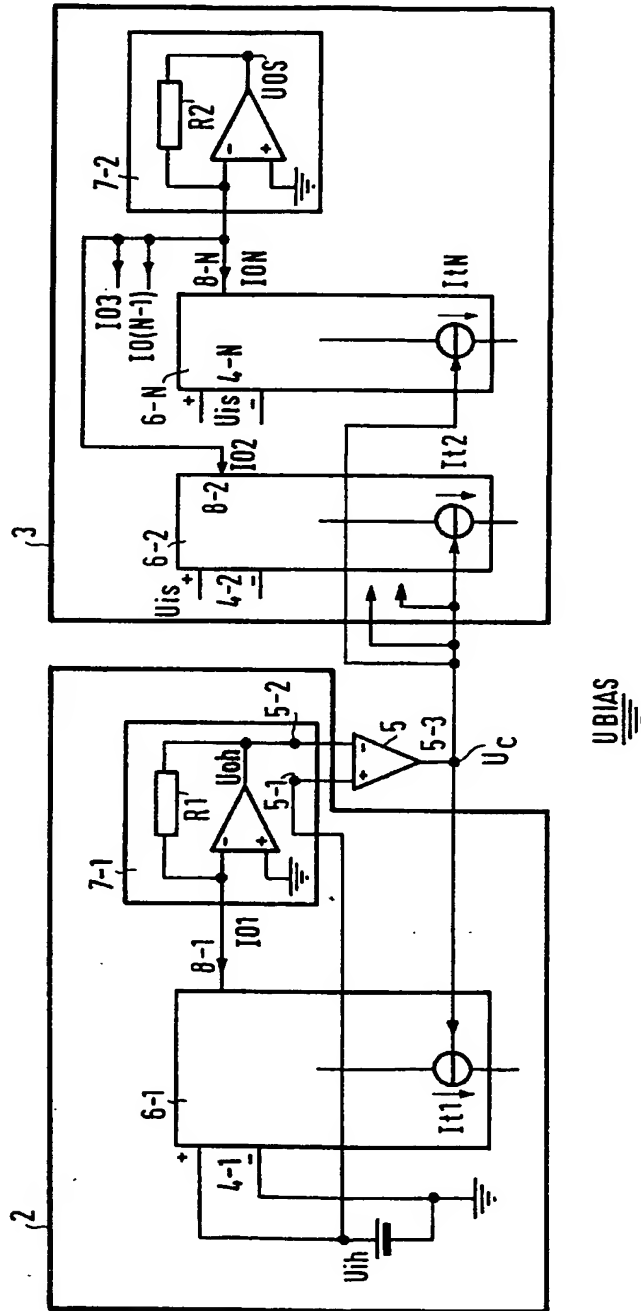


FIG.1

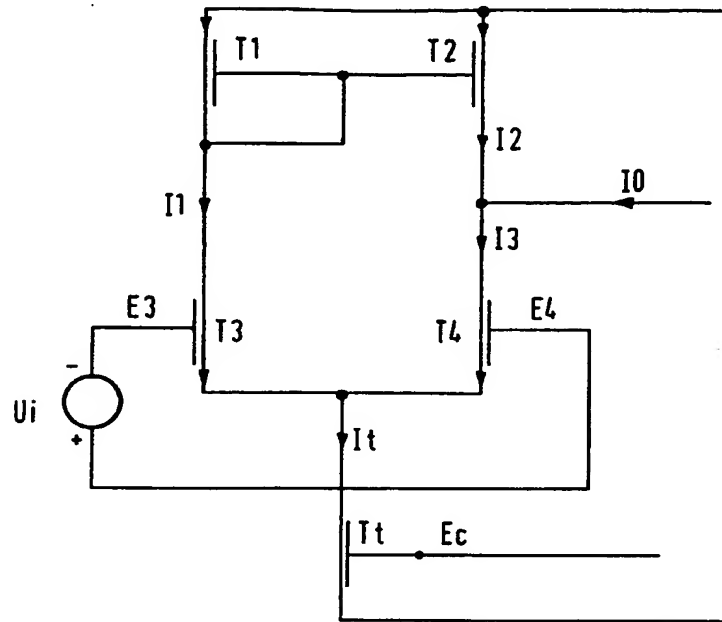


FIG.2

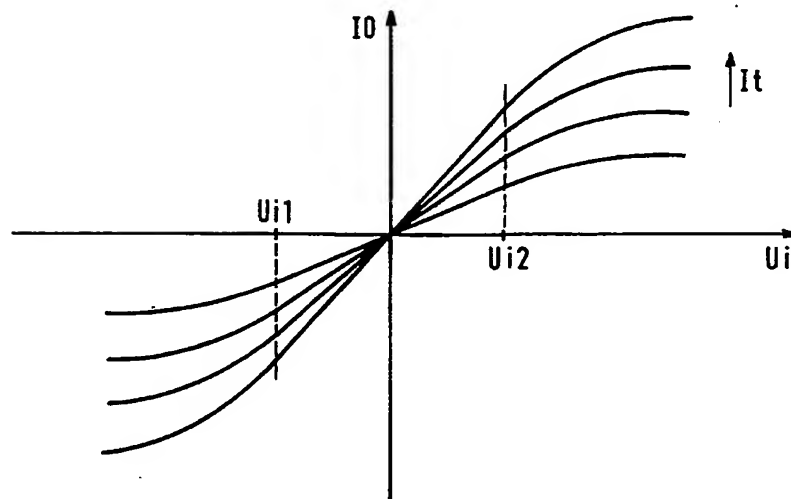


FIG.3



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EUROPEAN SEARCH REPORT

Application Number
EP 94 20 1563

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.5)
X	DE-A-41 01 892 (TELEFUNKEN ELECTRONIC) * the whole document *	1,2	H03F3/45 H03G1/00
D,A	US-A-4 489 282 (W. B. JETT) * column 1, line 39 - line 57 *	1	
A	PATENT ABSTRACTS OF JAPAN vol. 13, no. 463 (E-833) 19 October 1989 & JP-A-01 180 108 (TOSHIBA CORP) * abstract *	1	
			TECHNICAL FIELDS SEARCHED (Int.Cl.5)
			H03G H03F
The present search report has been drawn up for all claims			
Place of search		Date of completion of the search	Examiner
THE HAGUE		30 August 1994	Blaas, D-L
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